

# Factors Affecting the Limiting Oxygen Concentration Required for Ignition in an Aircraft Fuel Tank

by

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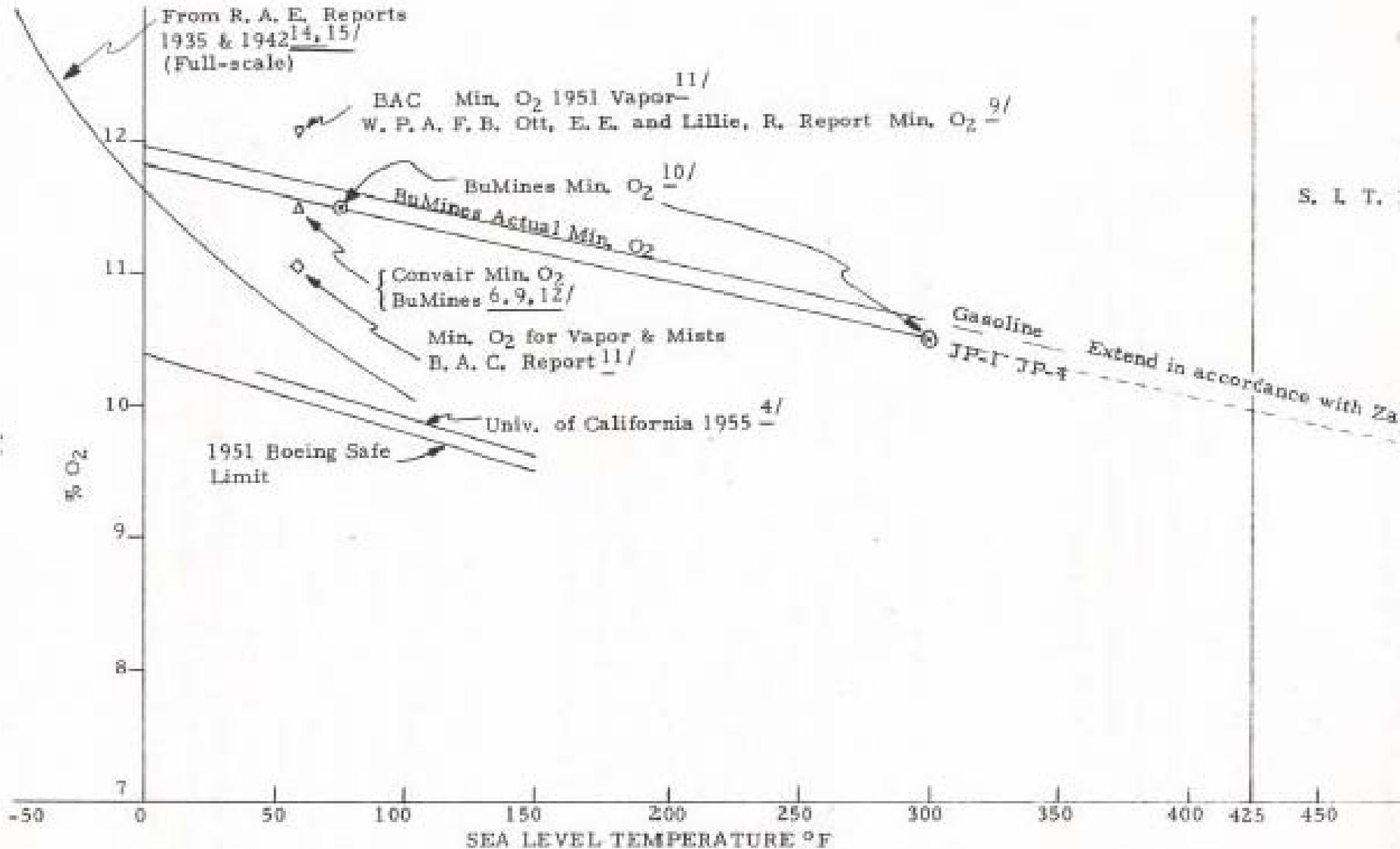
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# Background

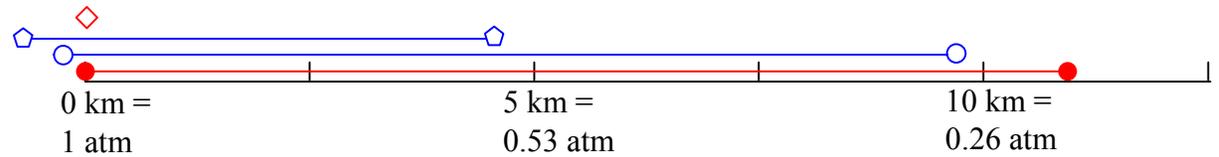
- LOC = Limiting Oxygen Concentration required for ignition during nitrogen inerting
- Used to be 9% based on old studies by Bureau of Mines and the military
- Recently changed to 12% based on:
  - Recent FAA LOC test data
  - Available inerting technology
  - Probabilistic argument on what is a sufficient level of safety improvement to the entire fleet
- This talk addresses factors affecting LOC test data

# Historical Data on LOC (from Zinn)

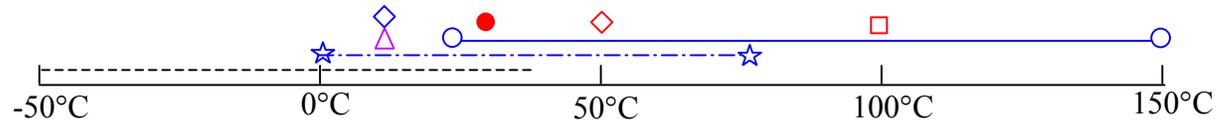


# Experimental Ranges

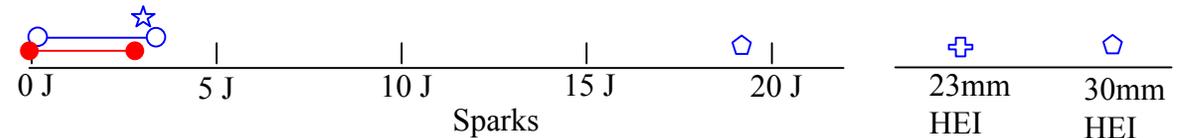
Altitude



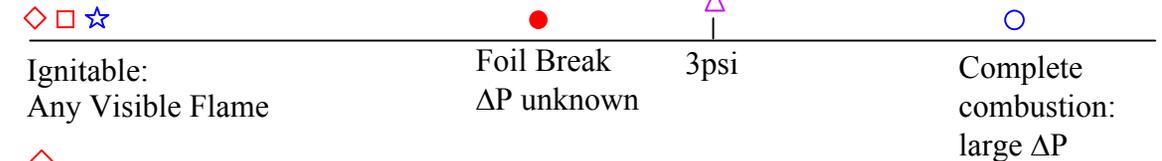
Ullage Temperature



Source Strength



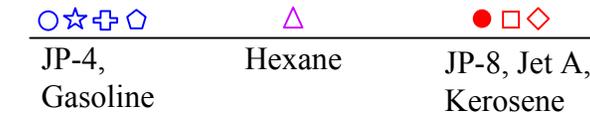
Ignition Criteria



Vibration, Slosh, and Mist

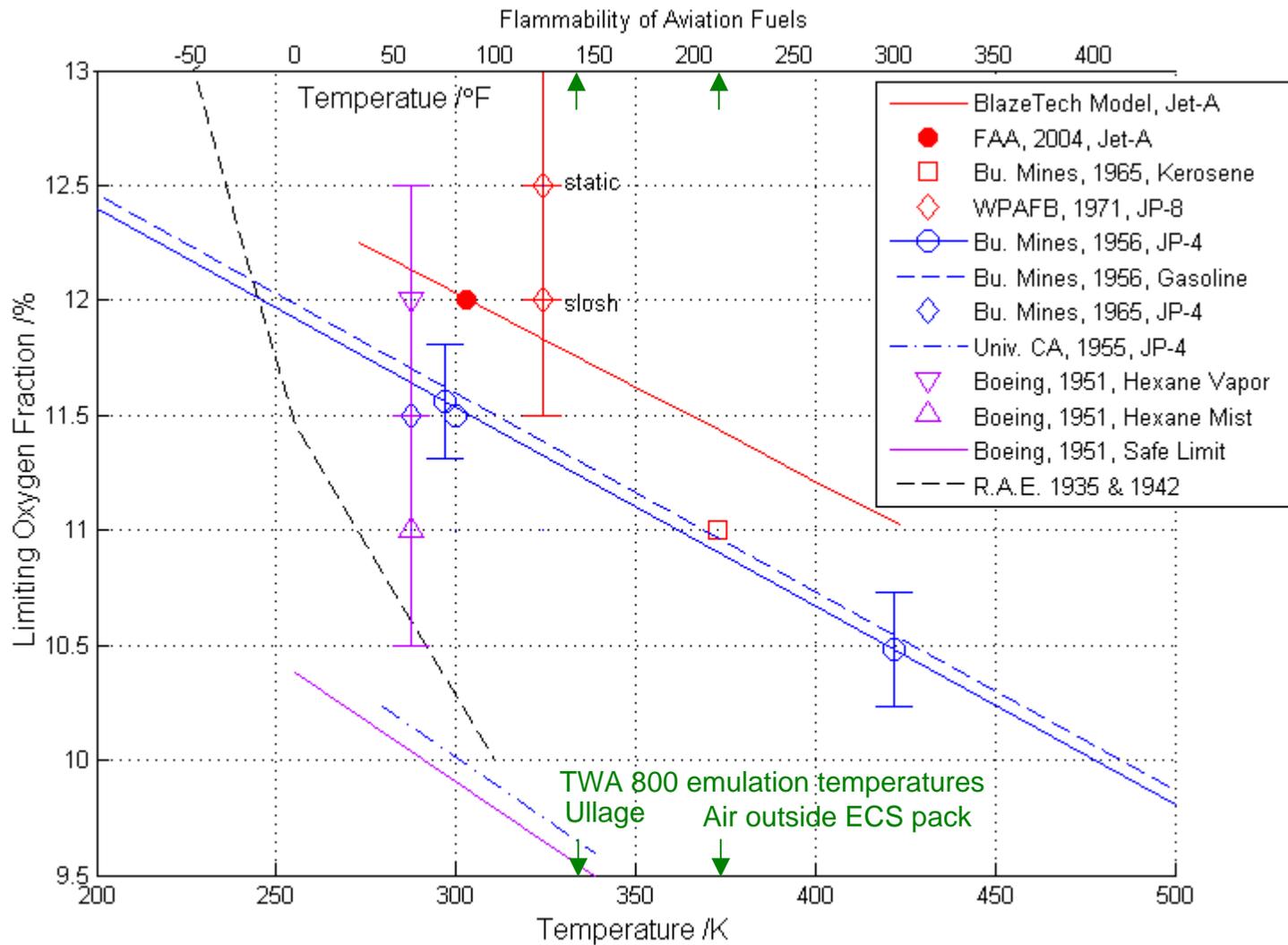


Fuel Composition



- FAA 2004
- Bu. Mines Kerosene 1965
- ◇ Ott WPAFB 1971
- Bu. Mines JP-4 1956
- ☆ U. CA 1955
- △ Boeing 1951
- ⊕ Anderson WPAFB 1978
- ◇ Tyson NWC 1991

# Historical Data on LOC



Revised from a graph compiled by Zinn, DOT/FAA-NA-71-26, 1971

# General Observations

- General agreement on effect of altitude
- Uncertainty in LOC data is +/- 0.5% for a given set of conditions with most experimental setups
- Recent FAA data agrees with old data
- BlazeTech model predicts correct dependence of LOC on ullage temperature
- No comment on R. A. E. since we could not find their report
- Many factors can decrease LOC below 12%

# Reported Drops in LOC below 12%

1. Source Strength/Ignition Criteria:
  - Effect: WPAFB  $\approx 0\%$ , Bu.Mines  $0.5\%$ , U.CA  $1.5\%$  (inc source)
  - Well covered by FAA study
2. Ullage Temperature:  $\approx 0.5\%$  if ullage at  $200^\circ\text{F}$
3. Vibration and slosh:
  - WPAFB used tank with slosh and vibration. Difference  $0.5\pm 0.5\%$ .
  - Boeing used hexane vapor and mist. Effect  $1\pm 0.5\%$
4. Gradients in Concentration: Depends on mixing.
  - U.CA  $1\pm 0.5\%$  with and without a fan to aid mixing
  - $\text{O}_2$  enters tank near vent
5. Variations in Jet A composition depending on grade:
  - $0.5\%$  between JP-4 and Jet A
  - Expect it to be less across various grades of Jet A

Combined Effect is neither obvious nor additive

# Model of Ullage Flammability – Overall Architecture

## Model Inputs

**Fuel Conditions:** type, amount & temperature

**Tank Geometry and dimensions**

**Ignition Characterization:** Source location, type and strength

**Flight Profile:** Altitude versus time, Fuel extraction rate to engine, and Fuel and tank wall temperatures

**Inerting:** ground vs. in-flight and percent concentration

**BlazeTank**

## Output

**Temp. and concentration vs. height and time**

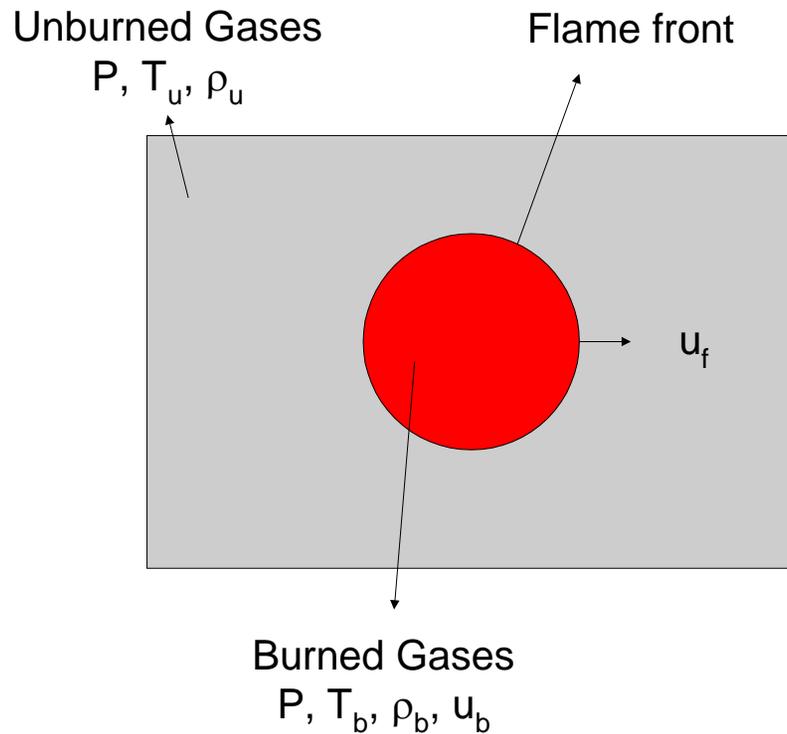
**Flammable volume inside fuel tank**

**Ignition and Propagation**

**If ignition occurs,** Temp., burn rate and Overpressure vs. time

**Limiting Oxygen Concentration**

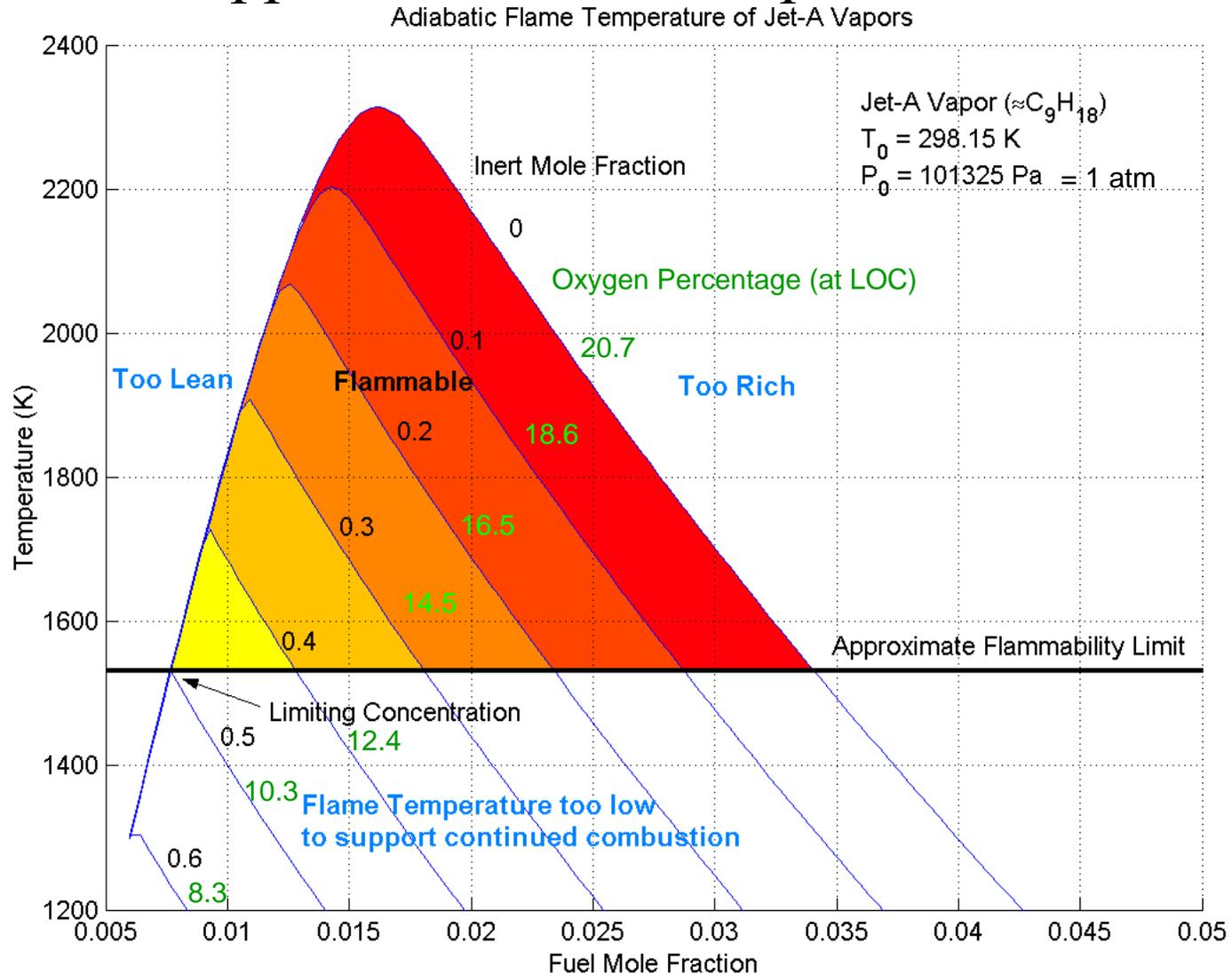
# Deflagration Module in BlazeTank



- Key assumptions
  - Ullage consists of 2 zones: premixed unburned gases and burned gases separated by a flame sheet
  - Unburned gases are pressurized by expanding burnt zone
  - Pressure in ullage remains spatially uniform because it equilibrates at acoustic speed  $\gg$  deflagration speed
- BlazeTank solves the coupled equations of:
  - Continuity
  - Energy conservation
  - Species conservation
  - Experimental burn rate (fuel, stoichiometry, T and P)

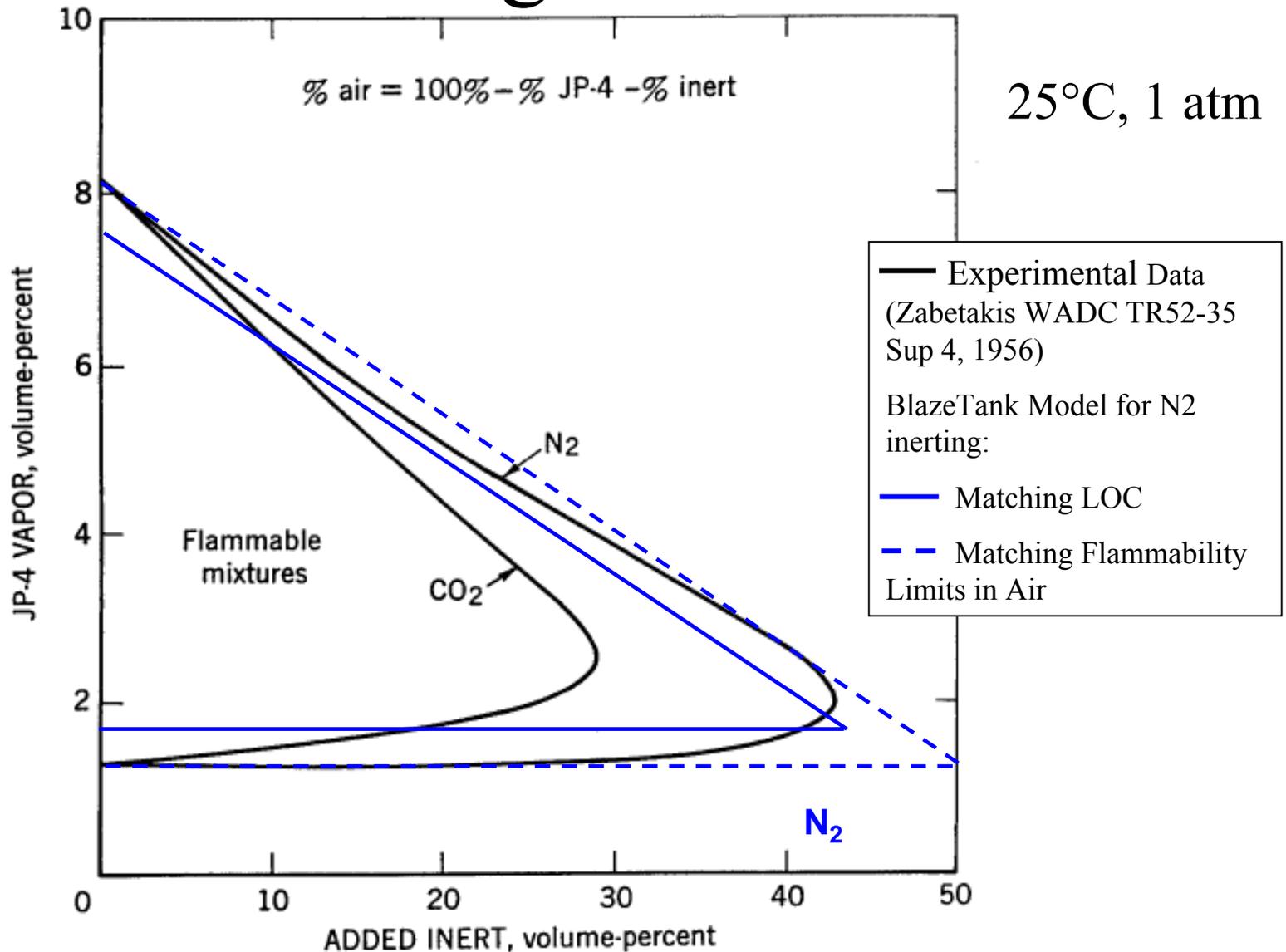
# LOC Predictions by BlazeTank

## First Approach: Flame Temperature Cut-off



Does not know the cut-off temperature a priori

# Inerting of JP-4



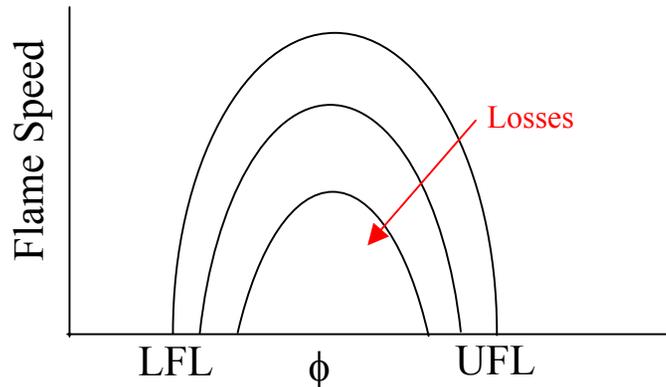
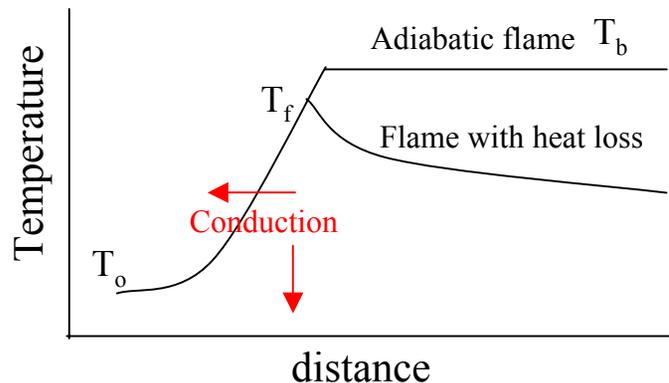
Doesn't match both LFL,UFL and LOC

# LOC Prediction by BlazeTank

## Second Approach: Zero Burning Velocity

If ullage cannot propagate a flame, it is not flammable

$U_f(\phi, T_a, T_b, Losses) = 0$ .  $\phi$ ,  $T_a$  known,  $T_b$  from equilibrium chemistry.  
Use lower flammability limit to determine the heat losses.



# Conclusions

- Recent FAA tests neglect key factors that can lower LOC:
  - Slosh and vibration, ullage temperature, variations in fuel composition and gradient effects
- Their combined effect is not obvious and may not be simply additive
- They can be quantified by testing or modeling (such as BlazeTank™)
- Modeling can be used to optimize:
  - The design of inerting systems
  - Their operation (when and how much to inert) so as to minimize load on engine
- Some inerting is better than none but one should err on the conservative side

# References

- Summer, “Limiting Oxygen Concentration Required to Inert Jet Fuel Vapors Existing at Reduced Fuel Tank Pressures”, DOT/FAA/AR-04/8, 2004
- Ott, E. and Lillie, R., “Influence of Fuel Slosh Upon the Effectiveness of Nitrogen Inerting for Aircraft Fuel Tanks”, AFAPL-TR-70-82, 1971
- Zabetakis, M. G. , Jones, G. W. , Scott, G. S. , and Furno, A. L., “Research on the Flammability Characteristics of Aircraft Fuels”, WADC Technical Report No.52-35, Supplement 4, January 1956.
- Zabetakis, M. G. , "Flammability Characteristics of Combustible Gases and Vapors, " U. S. Bureau of Mines Bulletin 627, 1965.
- Stewart, P. B. and Starkman, E. S. , "Inerting Conditions for Aircraft Fuel Tanks, " WADC Technical Report No.55-418, 1955
- Glendinning, B. A. and Parker, W. G., "Note on the Inhibition of Explosions in Fuel Vapour/Air Mixtures by Dilution With Nitrogen, " Royal Aircraft Establishment Chem Note No.515, August 1942.
- Gatward and Wifeth, "The Effect of Air Evolution From Fuel on the Inert Gas Protection of Aircraft Fuel Tanks, II Royal Aircraft Establishment T. N. No. M. E. 96, October 1951.
- Anderson, C.L., Test and Evaluation of Halon 1301 and Nitrogen Inerting Against 23 mm HEI Projectiles," AFFDL-TR-78-66, May 1978.
- Boeing Aircraft Company, "Explosive Limits of Fuel Vapors and Fuel Mists and the Suppression of These Limits With Inert Gases", WCNE MR 524-3079, 1951.
- Zinn Jr., S.V., “Inerted Fuel Tank Oxygen Concentration Requirements,” FAA-RD-71-42, August 1971.
- Tyson, J.H. and Barnes, J.F., “The Effectiveness of Ullage Nitrogen-Inerting Systems Against 30-mm High-Explosive Incendiary Projectiles-Final Report,” NWC TP 7129, May 1991.